



Choosing the Correct Capacitive Load Amplifier

Also refer to sales literature entitled, "Driving Capacitive Loads"

Introduction

In applications where an amplifier is used to drive either purely capacitive loads and/or loads that contain both capacitive and resistive elements, consideration must be given to the amplifiers output configuration and the continuous output current capability in order to achieve the required non-distorted output waveform. Distortion of the output waveform is particularly evident in applications requiring high peak-to-peak output voltage swings which can result in frequency limitations well below the gain-bandwidth capability of the amplifier if the corresponding output continuous current capability is not high enough to satisfy both the capacitive current and resistive current required by the load.

All Trek high voltage amplifiers are designed using class AB output driving stages and thus have the capability to both source and sink current to and from the capacitance associated with the load. Unfortunately, all output driving stages contain in itself a certain amount of capacitance (CINT) relative to ground (or other reference) which appears in parallel with the H.V. output terminal and thus in parallel with the load capacitance (C load). In addition, the capacitance (CW) associated with the wiring between the amplifiers output terminal and the load also appears in parallel with load capacitance thus the total capacitive load on the amplifier is equal to; $CT = CINT + CW + C \text{ LOAD}$.

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This application note deals with those applications where the amplifier's load is purely capacitive such as in beam steering or similar applications. The choice of the particular Trek amplifier model which best fits these applications can be determined using the five (5) step process shown below.

- 1) Prepare a list of amplifier candidates from those amplifiers shown in Chart A on the following page, which have an output peak to peak voltage capability required by the application.
- 2) Determine $CT - CINT$ by adding the anticipated wiring capacitance (CW) to the anticipated load capacitance (C LOAD) by direct measurement, calculation, or product data information such as pf/ft on coax cabling, capacitance data of the particular load used, etc.



Chart A

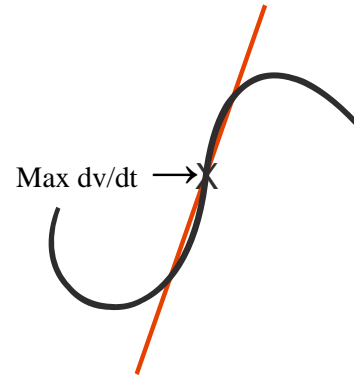
Model	Output Voltage (DC or Peak AC)	Internal Capacitance C int*	Output Current (DC or peak AC)
50/12	±50 kV	34 pF	±12 mA
40/15	±40 kV	43 pF	±15 mA
30/20A	±30 kV	50 pF	±20 mA
P0621 P or N	P: 0 to +30kV N: 0 to -30 kV	57pF	±20 mA
20/20C	±20 kV	60 pF	±20 mA
20/20C-HS	±20 kV	75 pF	±20 mA or ±60 mA peak AC for 1 ms
10/40A	±10 kV	60 pF	±40 mA
10/40A-HS	±10 kV	133 pF	±40 mA or ±60 mA peak AC for 1 ms
PD07016	±10 kV	60 pF	±60 mA or ±60 mA peak AC for 1 ms
664	±10 kV	110 pF	±20 mA
10/10B-HS	±10 kV	55 pF	±10 mA or ±50 mA peak AC for 1 ms
610E	±10 kV	66 pF	±2 mA
PD05034	±7.5 kV	50 pF	±50 mA or ±160 mA peak AC for 1 ms
609B-3	±10 kV	66 pF	±2 mA
5/80	±5 kV	70 pF	±80 mA
5/80-HS	±5 kV	160 pF	±80 mA or ±240 mA peak AC for 1 ms
609E-6	±4 kV	50 pF	±20 mA
PZD2000A	±2 kV	400 pF	±200 mA or ±400 mA peak AC
623B	±2 kV	50 pF	±40 mA
677B	±2 kV	330 pF	±5 mA
2220	±2 kV	300 pF	±10 mA
2210	±1 kV	300 pF	±20 mA
PZD700A	±700 V +1.4 kV or -1.4 kV	270 pF 135 pF	±100 mA ±50 mA
PZD700A M/S	±700 V +1.4 kV or -1.4 kV	530 pF 270 pF	±200 mA ±100 mA
2205	±500 V	300 pF	±40 mA
601C	±500 V or + 1 kV or -1 kV	400 pF	±10 mA DC or ±20 mA peak AC
PZD350A	+350 V	365 pF	±200 mA
PZD350A M/S	+ 700 V or -700 V	230 pF 730 pF 460 pF	±100 mA ±400 mA ±200 mA
2100 HF	±150 V	150 pF	±300 mA
603	±125 V or +250 V or -250 V	800 pF	±40 mA DC or ±80 mA peak AC

* [pF (pico farad = 10⁻¹²)]

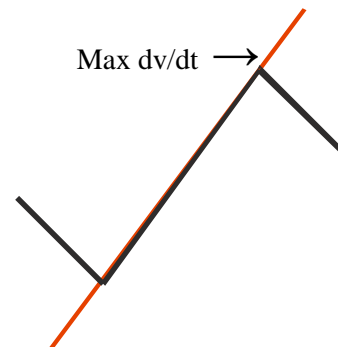
3) Determine the continuous current requirement (I_C) of the application by calculating $(I_C) = (C_T - C_{INT}) \times dv/dt$ where dv/dt is equal to the change of output voltage waveform per unit of time (which is waveform dependent)

ie:

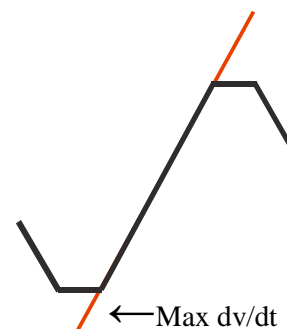
max dv/dt for sine wave = V peak-to-peak $\times \pi \times$ freq



max dv/dt for triangle wave = V peak-to-peak $\times 2 \times$ freq



max dv/dt for square wave = V peak to peak \times rise time





4. From the prepared list of amplifier candidates select those amplifier models from Chart A having a current capability equal to or greater than the continuous current requirement calculation of step 3.
- 5) For each model selected read the C_{INT} for that amplifier from Chart A and add that value of C_{INT} to the value of $C_T - C_{INT}$ in step 3 to obtain C_T the total capacitive load and recalculate the value of the continuous current requirement.
- 6) Choose the amplifier required based on the recalculated continuous current value requirement.

In addition, many Trek amplifiers have an additional feature which is very useful for driving capacitive loads. This feature allows the amplifier to deliver, over a specified time period, a current that has a peak value which is 2 to 3 times greater (depending upon the amplifier model) than the (I_C) value. This allows for very fast dv/dt rates and is particularly useful for square wave or pulse voltage applications where fast rise/fall time is required.